

## CONSERVATION LAWS (1)

### Quantities Conserved:

- Mass
- Momentum (Newton' Law)
- Energy (First Law of Thermodynamics)

### General Form:

$$Change = Production(Deconstruction)$$

### In Eulerian Frame:

$$Change|_{fixed\mathbf{x}} + Transport = Diffusion + Production$$

### Or:

$$\Phi_{,t} + \nabla \cdot \mathbf{v}\Phi = \nabla \cdot \mathbf{q} + S$$

# COMPRESSIBLE NAVIER-STOKES EQUATIONS (1)

Define:

$\rho$  : density  
 $v_i$ : fluid velocity in direction  $x_i$   
 $p$  : pressure  
 $e$  : specific total energy  
 $T$  : temperature  
 $q_i$ : heat flux in direction  $x_i$   
 $\sigma_{ij}$ : (deviatoric) stress tensor

Then: (L.M.H. Navier (1827), G.G. Stokes (1845))

$$\mathbf{u}_{,t} + \nabla \cdot \mathbf{F}^a = \nabla \cdot \mathbf{F}^v + \mathbf{S}$$

$$\mathbf{u} = \begin{Bmatrix} \rho \\ \rho v_i \\ \rho e \end{Bmatrix}, \quad \mathbf{F}_j^a = \begin{Bmatrix} \rho v_j \\ \rho v_i v_j + p \delta_{ij} \\ v_j (\rho e + p) \end{Bmatrix}, \quad \mathbf{F}_j^v = \begin{Bmatrix} 0 \\ \sigma_{ij} \\ v_l \sigma_{lj} - q_j \end{Bmatrix}$$

## COMPRESSIBLE NAVIER-STOKES EQUATIONS (2)

### State Equations

#### In General:

$$p = p(\rho, T)$$

#### Gases:

$$p = \frac{R}{m} \rho T = r \rho T$$

$R$  : Absolute Gas Constant

( $R = 8.312 \cdot m^2 kg / sec^2 \text{ } ^\circ K mol$ )

$m$  : Mass per mol

(Mass of 22.4 Liters of Gas at  $0^\circ C$  and  $760 mmHg$ )

Gas	$O_2$	$N_2$	$H_2$	Air
$m$ [ $g/mol$ ]	32	28.016	2.016	29
$c$ [ $m/sec$ ]	330	353	1316	347

## COMPRESSIBLE NAVIER-STOKES EQUATIONS (3)

$$\epsilon = e - \frac{1}{2}v_j v_j = c_v T$$

$\epsilon$  : Internal Energy

$c_v$ : Specific Heat at Constant Volume

$$h = \epsilon + \frac{p}{\rho} = c_p T$$

$h$ : Enthalpy

$c_p$ : Specific Heat at Constant Pressure

$\Rightarrow$  For **Ideal** Gases:

$$p = (\gamma - 1)\rho[e - \frac{1}{2}v_j v_j]$$

$\gamma$ : Ratio of Specific Heats ( $= c_p/c_v$ )

Valid up to 800K (Molecular Vibration)

## COMPRESSIBLE NAVIER-STOKES EQUATIONS (4)

### Viscous Stress Tensor

$$\sigma_{ij} = \mu \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right) + \lambda \frac{\partial v_k}{\partial x_k} \delta_{ij}$$

- So-Called Newtonian Fluid
- In General:  $\sigma_{ij} = \sigma_{ij}(\nabla \mathbf{v})$

### Stokes Hypothesis:

$$\lambda = -\frac{2\mu}{3}$$

### Sutherland's Law:

$$\frac{\mu}{\mu_\infty} = \left( \frac{T}{T_\infty} \right)^{\frac{3}{2}} \cdot \frac{T_\infty + 110}{T + 110}$$

- Valid for gases

## COMPRESSIBLE NAVIER-STOKES EQUATIONS (5)

Fourier's Law:

$$\mathbf{q} = -k\nabla T$$

$k$ : conductivity

For Gases:

$$\frac{k}{k_{\infty}} = \frac{\mu}{\mu_{\infty}}$$

**COMPRESSIBLE NAVIER-STOKES EQUATIONS (6)**Entropy:  $s$ 

$$Tds = de + pd\left(\frac{1}{\rho}\right) = dh - \frac{dp}{\rho}$$

 $\Rightarrow$ 

$$Tds = c_p \left( dT - \frac{\gamma - 1}{\gamma} \frac{T}{p} dp \right)$$

 $\Rightarrow$ 

$$s - s_0 = c_p \left( \ln\left(\frac{T}{T_0}\right) - \frac{\gamma - 1}{\gamma} \ln\left(\frac{p}{p_0}\right) \right)$$

 $\Rightarrow$  For Isentropic Flows ( $ds = 0$ ):

$$\frac{p}{p_0} = \left( \frac{\rho}{\rho_0} \right)^\gamma$$

 $\Rightarrow$  With  $p = r\rho T$ ,  $h = c_p T$ :

$$\frac{h}{h_0} = \frac{T}{T_0} = \left( \frac{\rho}{\rho_0} \right)^{\gamma-1}$$

## COMPRESSIBLE NAVIER-STOKES EQUATIONS (7)

Speed of Sound:

$$c^2 = \left( \frac{\partial p}{\partial \rho} \right)_s = \gamma \frac{p}{\rho} = (\gamma - 1) c_p T = (\gamma - 1) h$$

Iso-Enthalpic Flows Revisited:

$$h = c_p T + \frac{\mathbf{v}^2}{2} = c_p T_0$$

$T_0$ : Stagnation Temperature

$$\begin{aligned} T_0 &= T \cdot \left( 1 + \frac{\mathbf{v}^2}{2c_p T} \right) = T \cdot \left( 1 + \frac{(\gamma - 1)\mathbf{v}^2}{2\gamma \frac{p}{\rho}} \right) \\ &= T \cdot \left( 1 + \frac{\gamma - 1}{2} M^2 \right) \end{aligned}$$

$M$ :  $= |\mathbf{v}|/c$ : Mach-Number



## COMPRESSIBLE NAVIER-STOKES EQUATIONS (8)

Isentropic Flows:

$$\frac{\rho}{\rho_0} = \left( \frac{h}{h_0} \right)^{\frac{1}{\gamma-1}} = \left( 1 - \frac{\mathbf{v}^2}{2h_0} \right)^{\frac{1}{\gamma-1}}$$

and:

$$c^2 = \gamma \frac{p}{\rho} = (\gamma - 1)h = (\gamma - 1)\left(h_0 - \frac{\mathbf{v}^2}{2}\right)$$

## NON-DIMENSIONAL FORM (1)

Aim: Establish Similarity for Flows

How: Define Reference Quantities

- Inflow Quantities
- Internal Characteristic Quantities

Typically:

$L$  : Characteristic Length

$|\mathbf{v}_\infty|$  : Inflow/Free-Stream Velocity

$\rho_\infty$  : Inflow/Free-Stream Density

$T_\infty$  : Inflow/Free-Stream Temperature

$\mu_\infty$  : Inflow/Free-Stream Viscosity

$k_\infty$  : Inflow/Free-Stream Conductivity

## NON-DIMENSIONAL FORM (2)

Define Non-Dimensional Quantities:

$$t^* = \frac{t |\mathbf{v}_\infty|}{L} \quad , \quad x_i^* = \frac{x_i}{L} \quad , \quad v_i^* = \frac{v_i}{|\mathbf{v}_\infty|}$$

$$\rho^* = \frac{\rho}{\rho_\infty} \quad , \quad T^* = \frac{T}{T_\infty} \quad , \quad p^* = \frac{p}{\rho_\infty |\mathbf{v}_\infty|^2} \quad , \quad e^* = \frac{e}{|\mathbf{v}_\infty|^2}$$

$$\mu^* = \frac{1}{Re_{\infty,L}} \cdot \frac{\mu}{\mu_\infty} \quad , \quad k^* = \frac{1}{(\gamma - 1) M_\infty^2 Pr Re_{\infty,L}} \cdot \frac{k}{k_\infty}$$

## NON-DIMENSIONAL FORM (3)

### Characteristic Numbers:

$$Re_{\infty,L} = \frac{\rho_{\infty} |\mathbf{v}_{\infty}| L}{\mu_{\infty}}: \text{Reynolds-Number};$$

Ratio of: Inertial Forces:Viscous Forces

$$M_{\infty} = \frac{|\mathbf{v}_{\infty}|}{c_{\infty}}: \text{Mach-Number};$$

Ratio of: Fluid Velocity:Speed of Sound

$$Pr_{\infty} = \frac{c_p \mu_{\infty}}{k_{\infty}}: \text{Prandtl-Number};$$

Ratio of: Viscosity:Conductivity

$$\gamma = \frac{c_p}{c_v}:$$

Ratio of: Specific Heat at Constant Pressure:  
Specific Heat at Constant Volume

## NON-DIMENSIONAL FORM (4)

By Going to Dimensionless Form, Dropping the  $*$ :

$$\mathbf{u}_{,t} + \nabla \cdot \mathbf{F}^a = \nabla \cdot \mathbf{F}^v + \mathbf{S}$$

$$\mathbf{u} = \begin{Bmatrix} \rho \\ \rho v_i \\ \rho e \end{Bmatrix}, \quad \mathbf{F}_j^a = \begin{Bmatrix} \rho v_j \\ \rho v_i v_j + p \delta_{ij} \\ v_j(\rho e + p) \end{Bmatrix}, \quad \mathbf{F}_j^v = \begin{Bmatrix} 0 \\ \sigma_{ij} \\ v_l \sigma_{lj} - q_j \end{Bmatrix}$$

$$p = (\gamma - 1)\rho[e - \frac{1}{2}v_j v_j]$$

$$\sigma_{ij} = \frac{1}{Re}\mu \left( \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} - \frac{2}{3} \frac{\partial v_k}{\partial x_k} \delta_{ij} \right)$$

$$\mathbf{q} = -\frac{1}{Pr Re} k \nabla T$$

## TYPICAL PARAMETERS AT 20° C

Fluid	$\rho$ [ $kg/m^3$ ]	$\mu$ [ $kg/m/sec$ ]	$\nu$ [ $m^2/sec$ ]	$Pr$
Water	1000	$1.00 \cdot 10^{-3}$	$1.00 \cdot 10^{-6}$	7.030
Glycerine			$6.80 \cdot 10^{-4}$	
Mercury			$1.00 \cdot 10^{-7}$	0.023
Lubr. Oil			$8.92 \cdot 10^{-4}$	10-100
Air	1.21	$1.79 \cdot 10^{-5}$	$1.50 \cdot 10^{-5}$	0.710

## TYPICAL REYNOLDS NUMBERS

Object	L [ <i>m</i> ]	V [ <i>m/sec</i> ]	<i>Re</i>
Protozoa	.001	0.01	$1.00 \cdot 10^1$
Piranha	0.15	0.30	$4.50 \cdot 10^4$
Manta-Ray	2.50	0.50	$1.25 \cdot 10^6$
Penguin	1.00	5.00	$5.00 \cdot 10^6$
White Shark	4.00	3.00	$1.20 \cdot 10^7$
Tuna	3.00	10.0	$3.00 \cdot 10^7$
Blue Whale	30.0	1.00	$3.00 \cdot 10^7$
Butterfly	0.05	4.00	$1.30 \cdot 10^4$
Albatros	0.30	10.0	$2.00 \cdot 10^5$
Car (Sedan)	4.00	25.0	$6.60 \cdot 10^6$
Truck	25.0	25.0	$4.20 \cdot 10^7$
B-747 WTO	6.00	40.0	$1.60 \cdot 10^7$
B-747 WCR	6.00	220.	$8.80 \cdot 10^7$
SR-71	20.0	2220	$2.90 \cdot 10^9$

## LIMIT OF VALIDITY OF CONTINUUM APPROXIMATION

Define: Knudsen-Number

$$Kn = \frac{\text{Mean Free Path}}{\text{Characteristic Length}} \approx \frac{M_\infty}{Re_{\infty,L}}$$

For  $Kn \leq 0.03$ : Continuum Approximation Very Good

Exceptions:

- Large Mean Free Paths
  - Reentry Flows
- Small Characteristic Lengths
  - Micromachines