

Performance of a Pillow Plate Thermosiphon Reboiler for Hexanol, Pentanol, and their Mixtures

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Pillow Plate Heat Exchangers (PPHEs)

- more compact than shell and tube HEs & more temperature- and pressure-resistant than plate HEs
 - advantageous usage as thermosiphon reboiler (TR): stabilized natural circulation & enhanced operating ranges towards low pressures, low submergences, and small driving temperature differences [1]
 - lack of experimental data and model for PPHEs, especially for mixtures
- Aim: determining the performance of a PPTR for pure substances and mixtures

Experimental Result

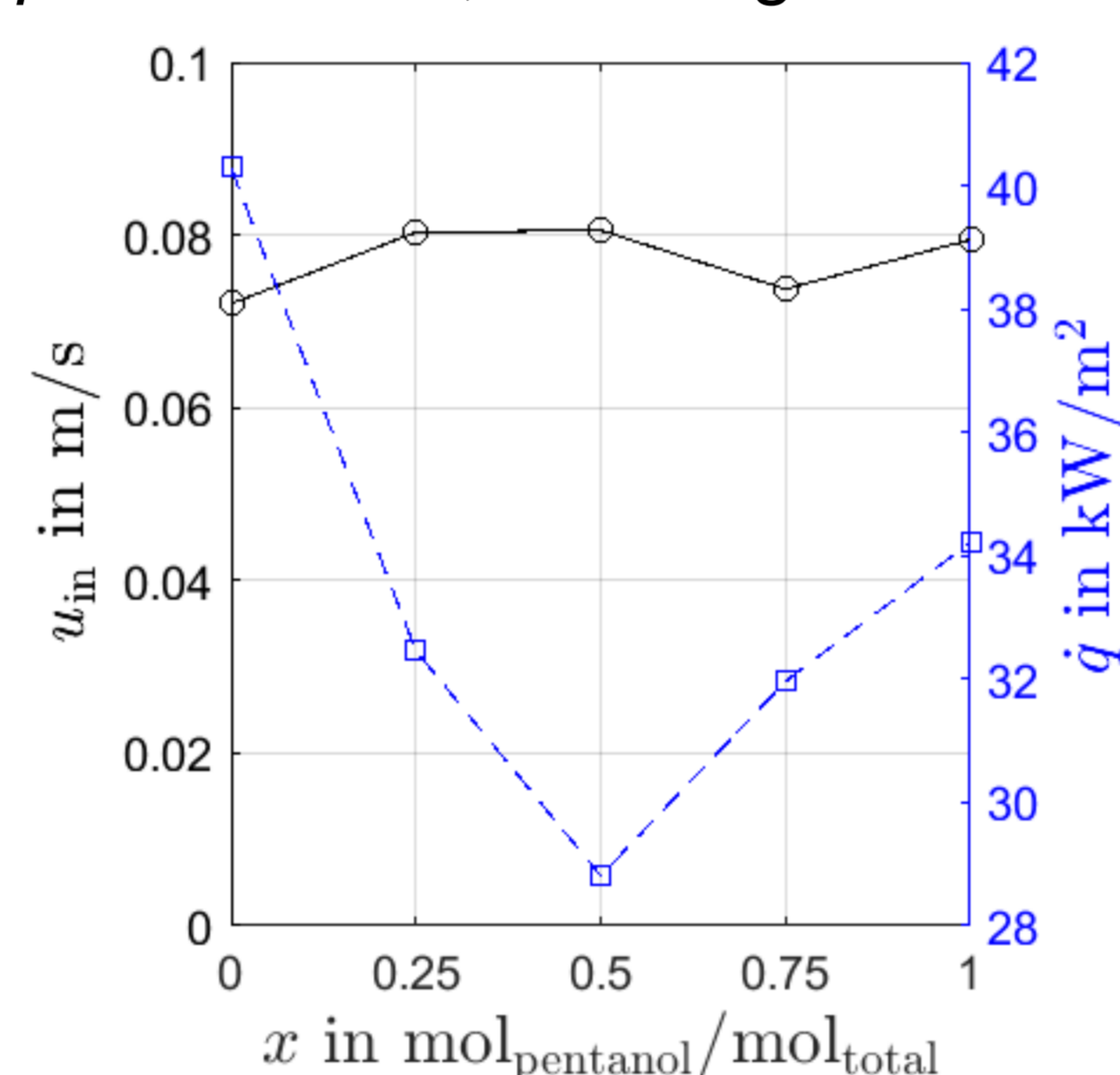
Fluid dynamics: Inlet velocity

- barely influenced by varying pentanol fractions
- main cause: similar density

Thermal performance: Heat flow density

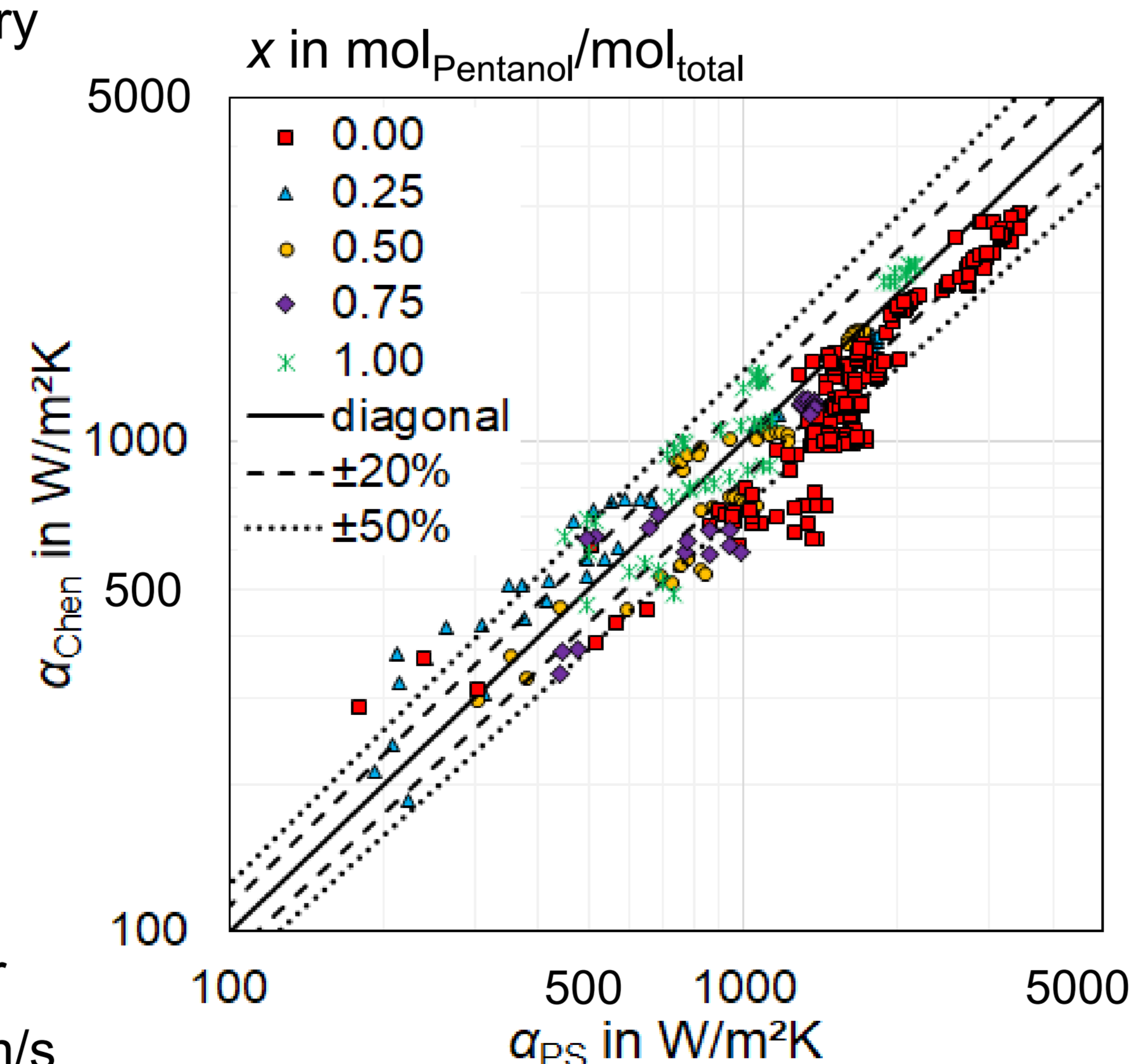
- hexanol > pentanol > mixture
- minimum at $x = 0.5 \text{ mol}_{\text{pentanol}}/\text{mol}_{\text{total}}$
- main cause: the enrichment of the lower boiling component in the vapor phase is highest for intermediate compositions of the mixtures [2]

Operating conditions: $\Delta T = 20 \text{ K}$,
 $p = 800 \text{ mbar}$, submergence 90%



Heat transfer modeling

- using equivalent tube bundle geometry
- $1/\alpha_{(PS)} = 1/k - 1/\alpha_{HS} - s/\lambda_{wall}$
with $k = \frac{\dot{Q}}{A \cdot \Delta T}$, $\Delta T = T_{HS} - \bar{T}_{PP}$,
and α_{HS} according to [2]
- Bennet&Chen's model [3]
 $\alpha_{Bennet\&Chen} = S \cdot \alpha_{nb} + F \cdot \alpha_{fc}$
nb: nucleate boiling [2]
fc: forced convection [3]
- mean absolute percentage deviation
 $= \frac{100\%}{n} \cdot \sum \left| \frac{\alpha_{Bennet\&Chen} - \alpha_{PS}}{\alpha_{PS}} \right| = 17\%$
validity range:
 $7 \text{ K} \leq \Delta T < 21 \text{ K}$, $0.1 \text{ bar} \leq p \leq 1.0 \text{ bar}$
 $\dot{q} \leq 47 \text{ kW/m}^2$, $0.02 \text{ m/s} \leq u_{in} < 0.12 \text{ m/s}$



Bennet&Chen's model is **Why?** The single-phase zone is negligible small due to low height and low pressure loss of PPs
capable for PP TRs

Experimental Setup

pillow plate (PP):

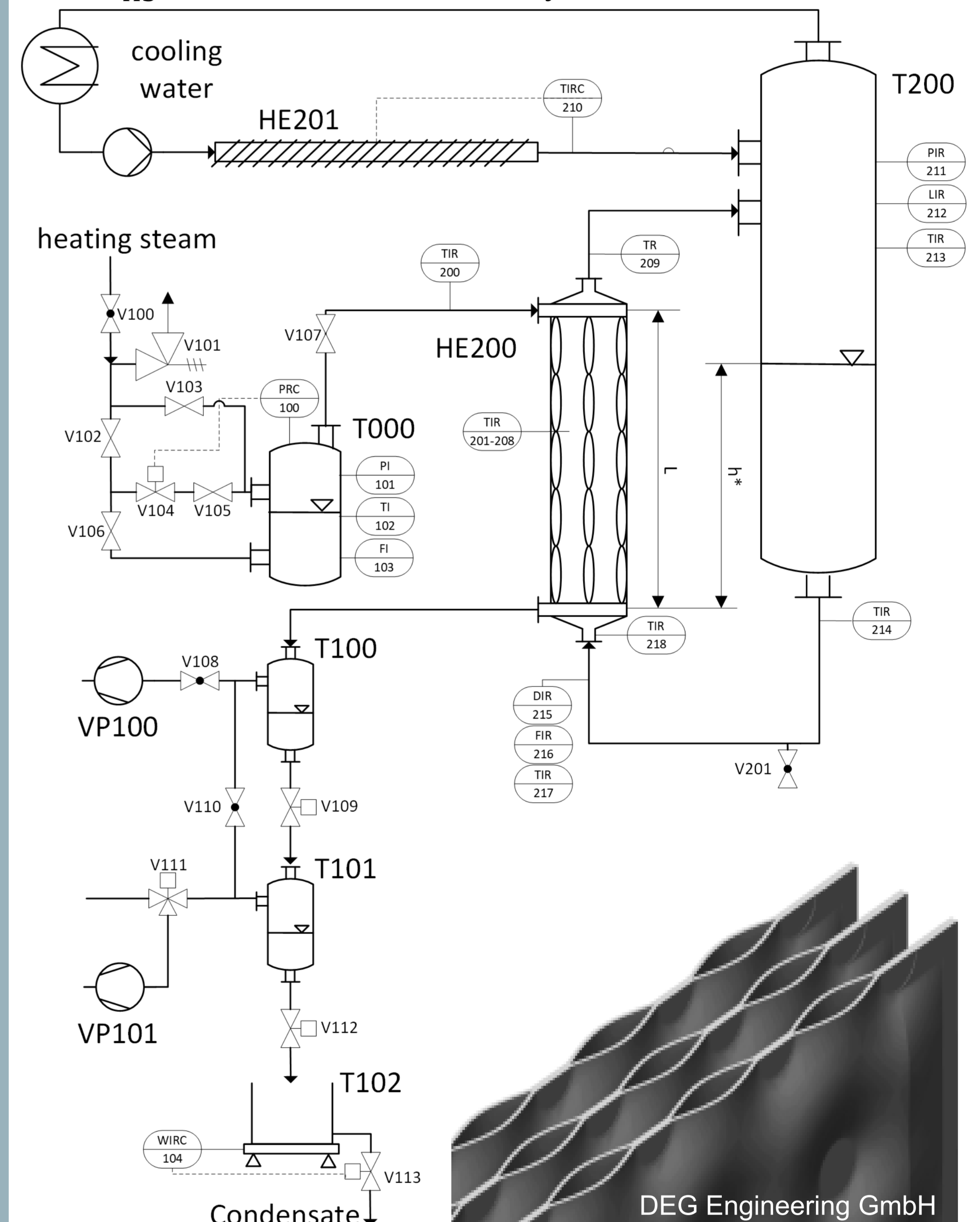
- one double-sided + two single-sided expanded plates
- material SS 1.4571, $L \times B = 800 \times 220 \text{ mm}^2$,
- $d_h = 17.51 \text{ mm}$, $A_{ht} = 0.704 \text{ m}^2$ [1]

product side (PS):

- self-circulation through the gaps between PPs
- pressure 100 - 1000 mbar, submergence 30% - 130%

heating side (HS):

- heating steam inside PP
- $T_{HS} : 65 \dots 180 \text{ }^\circ\text{C}$, heat duty: 5 ... 30 kW



Literature

- [1] R. Goedecke, S. Scholl, *Heat Mass Transf.* 2019, 55(1), 95–104.
- [2] P. Stephan, S. Kabelac, M. Kind, D. Mewes, K. Schaber, T. Wetzel (Eds.), 12. ed., Springer Vieweg, Berlin, Heidelberg, 2019.
- [3] D.L. Bennet, J.C. Chen, Correlation for Boiling Heat Transfer to Saturated Fluids in Convective Flow, *Ind. Eng. Chem. Eng. J.* 26, 454-462, 1980.

Conclusions and Outlook

- Fluid dynamics and thermal performance of PPTRs are differently influenced by varying pentanol fractions.
- The heat transfer in the gaps between PPs can be calculated using equivalent tube bundle geometry and Bennet&Chen's model of flow boiling.
- Investigation of further mixtures e.g. water - ethylene glycol